

PATENT SPECIFICATION

DRAWINGS ATTACHED

833,382



Date of Application and filing Complete Specification Sept. 30, 1957.

No. 30510/57.

Application made in United States of America on Oct. 8, 1956.

Complete Specification Published April 21, 1960.

Index at acceptance: —Class 97(1), B7G.

International Classification: —G02b.

COMPLETE SPECIFICATION

Improvements in Achromatic Optical Systems

We, BAUSCH & LOMB OPTICAL CO., a corporation organised under the laws of the State of New York, United States of America, of 635, St. Paul Street, Rochester, New York,

5 United States of America, do hereby declare the invention, for which we pray that a patent may be granted to us, and the method by which it is to be performed, to be particularly described in and by the following statement:

10 This invention relates to an achromatic optical system and particularly to a system for achromatizing prisms by the use of diffraction grating means for performing the achromatization.

15 Many types of optical apparatus, such as large gunsights, range finders, etc., require optical prisms or wedges that are achromatic with respect to transmitted light. Heretofore, 20 these requirements have been met by prismatic type compensators which have the disadvantages of being bulky and expensive and have a relatively small deviation of transmitted light. These disadvantages may be completely 25 overcome when the prisms are achromatized by combining diffraction gratings with prisms in a specified manner. For best use, the achromatizing means should not only be capable of completely achromatizing transmitted light 30 but should also be easily adaptable to the correction of a wide variety of chromatic aberrations in prisms.

It is an object of this invention to provide 35 achromatization of a prism by light diffracting means and furthermore to provide by this means an uncommonly large deviation of the line of sight in optical instruments which use achromatized prisms.

Another object of this invention is to provide 40 achromatization of a prism by combination therewith of a diffraction grating whereby the achromatized prism is light in weight, and is compact and small in size for installation in restricted spaces.

45 It is a further object to provide such an [Price 3s. 6d.]

achromatized prism for completely neutralizing all parts of the transmitted spectrum, the achromatizing means being effective to entirely achromatize various prisms which have spectrally different chromatic aberrations.

50 The present invention accordingly provides an achromatic system comprising a light dispersing prism, a pair of diffraction gratings spaced from each other and positioned in optical alignment with said prisms, the blaze of one grating being deviated in an opposite direction to the blaze of the other grating to produce a residual dispersion which substantially compensates for the dispersion of the prism.

55 Further objects and advantages will be apparent in the details of construction and the arrangement and combination of parts as hereinafter described in the specification and shown in the accompanying drawing in which:—

60 Fig. 1 is a diagrammatic view of an achromatically corrected prism incorporating the principles of this invention,

65 Fig. 2 is a perspective view partly broken away and shown in section, of one form of the invention,

70 Fig. 3 is a vertical sectional view of another form of the invention,

75 Fig. 4 is a vector diagram explanatory of Fig. 2, and

80 Fig. 5 is a vertical sectional view of a compensator embodying the construction shown in Fig. 1.

85 This invention is based on certain well-known properties of gratings and prisms, one being that diffraction gratings disperse transmitted light in an opposite manner to glass prisms, i.e., a grating deviates red light more than blue light whereas a prism deviates blue light more than red light.

90 As shown diagrammatically in Fig. 1, this invention typically comprises an achromatic system generally indicated at 10 which includes a first diffraction grating indicated at 11 and

50

55

60

65

70

75

80

85

90

Price 25p

- a second diffraction grating indicated at 12, the grating surface of each being mounted substantially parallel with a refracting surface 13 of a prism 14 to be achromatized. The 5 diffraction gratings 11 and 12 are positioned in optical alignment with the prism 14, optical alignment being defined as the operative alignment of a plurality of optical parts such that a beam of light will pass serially through each 10 individual part in succession. For the sake of reducing the overall size of the device, a Fresnel type prism 14 is preferred and illustrated, although a regular prism 14' as shown in Fig. 3 may be used with equal effect.
- 15 According to one form of this invention, the grating constant, i.e., the number of lines per millimeter in the ruling, pertaining to diffraction grating 11 is greater than the grating constant of diffraction grating 12 and consequently 20 grating 11 produces greater deviation of the transmitted spectrum. The rulings of gratings 11 and 12 are arranged with their line structures, i.e., the lines on the grating surface that are formed by the rulings, parallel to each other and parallel to the line or groove 25 structure of the Fresnel prism 14. If an ordinary three-sided prism is used instead of the Fresnel prism 14 such as shown at 14' in Fig. 3 of the drawing, said rulings are arranged parallel to the base of the prism. Said gratings should not be in optical contact 30 with each other although the thickness of the airspace therebetween is not critical.
- The gratings 11 and 12 are specially blazed 35 to produce the results described hereinafter, a "blaze" being defined as the maximum light energy line that is found in a spectrum formed by a grating. Currently, diffraction gratings are "blazed" by controlling the groove face angle of the ruling so as to concentrate the transmitted spectral energy in the desired region of the spectrum. Therefore, the term "blazing" may be defined as being the art of controlling the distribution of energy which 40 comes from the grating by controlling the contours or face angles of its ruled grooves. The "blaze" accordingly governs the direction in which the transmitted energy is concentrated and in this invention the grating is 45 blazed to produce maximum energy in the first order spectrum, this energy being preferably concentrated on one side of the zero order as illustrated in Fig. 1. It is also possible to form the grating so that the second order 50 maxima are as great as the first order maxima so that that order may be used. The invention is therefore not limited to the use of light in the first order only.
- It is important that the "blaze" of the 55 respective gratings 11 and 12 be arranged in opposite directions to each other as indicated by the arrows "b" and "c" in Fig. 1 whereby the respective dispersions of the gratings will act in opposition to each other 60 to produce what is called a "residual dispersion". The residual dispersion may be defined as the algebraic sum of the dispersions of the gratings 11 and 12 when the dispersion of grating 11 is considered positive and the other dispersion is considered negative. Two of such diffracted spectra are shown at 15 and 16 in Fig. 1, the blue end and the red end of each spectrum being designated B and R, respectively. At the second grating 12, said spectra are rediffracted to form the spectra 15' and 16' which enter the Fresnel prism 14 in a condition of dispersion which just matches the dispersion of the prism so that white light is transmitted thereby. 70
- With respect to one specific operative example of this form of the invention, light is assumed to enter the grating 11 at normal incidence from the left in Fig. 1. The grating 11 which is ruled at 300 lines per millimeter produces a deviation of the diffracted first order spectra 15 and 16 which is $11^\circ 21' 18.1''$ for red light designated by R, and $8^\circ 23' 8''$ for blue light designated by B. 75
- The diffracted spectra 15 and 16 are rediffracted by the diffraction grating 12 which is ruled at 273.9 lines per millimeter and is placed so that its blaze is opposite end parallel to that of grating 11. The beams 15' and 16' emerging from the grating 12 are deviated less than the deviation that is provided by the grating 11, the beams being partially reunited so that those spectra are then deviated closer to "normal incidence", the deviation angles being only $0^\circ 47' 32''$ and $0^\circ 35' 17''$ for red and blue light, respectively. This deviation substantially compensates for the dispersion of the Fresnel prism 14 which has an angle "a" of 22° between the refractive surfaces and is made from glass having a dispersion 80
- $\gamma = \frac{n_0 - 1}{n_p - n_c} = 57.8.$
- The difference between the grating constants 300 and 273.9 relative to the gratings 11 and 12, is precalculated to produce said residual dispersion of the spectra 15' and 16'. Consequently, the gratings 11 and 12 and prism 14 comprise a combination of optical elements which cooperatively produce deviated color-free, white light. 90
- A preferred commercial form of this invention is shown diagrammatically in Fig. 2 of the drawing wherein the residual dispersion for achromatizing the prism is secured in a different manner. According to this form of the invention, two similar diffraction gratings 22F and 22R, located in front and rear positions, respectively, and each having the same grating constant or periodicity of ruling, and placed with their ruled surfaces parallel to each other and parallel to a plane which passes through the apex of angle "a" Fig. 1, between the entrance and exit surfaces of a Fresnel prism 23, similar to the prism 14. 100

- An ordinary triangular prism 14¹ may be substituted for the Fresnel prism 23 as shown in Fig. 3 if desired, in which case said ruled surfaces are both positioned parallel to a single plane which passes through the apex of the included angle a^1 between the entrance and exit refractive surfaces on that prism. In Fig. 2, the line or groove structure of the prism 23 is indicated by the shade lines 24 and it will be noted that the gratings 22F and 22R may be rotated during assembly individually in opposite directions from a neutral or zero deflection position through an angle α relative to the lines 24 to position the line 2 structures of the respective gratings at an angle α to each other. Said angle α is pre-calculated as explained hereinafter so that when the gratings 22F and 22R are positioned in this manner with the blaze of one grating arranged in an opposite direction to the blaze of the other grating, the dispersion of the Fresnel prism 23 is substantially compensated. The resultant deviation of the spectra by the gratings 22F and 22R does not lie in a plane perpendicular to the line structure of either of said gratings but only the perpendicular component of the deviation of grating 22R opposes the deviation of the grating 22F, considering the individual deviations as vector quantities. The combined effect of the diffractions produced by the mutual inclination and opposition of the respective rulings is to yield a residual dispersion which is equal and opposite to the dispersion of the prism 23 and also matches its spectral quality.
- To specifically elucidate the preferred form of the invention, the analytical and computational procedure for obtaining constructional data for a typical achromatized system having two like gratings 22F and 22R and a piston is given hereinbelow.
- The deviation for the various wavelengths of light by a given grating is obtained by the mathematical expression,
- $$(A) \quad \sin \Delta = \frac{\lambda + e \sin \theta}{e}$$
- wherein, Δ = deviation of grating for wavelength λ
 e = grating constant
 θ = angle of incidence of light on grating
 λ = wavelength of light
- When the two similar gratings 22F and 22R are combined, their resultant deviation may be graphically shown by the vector diagram of Fig. 4 in which,
- δ = the resultant deviation
 - Δ = deviation of either grating alone
 - α = angle between the line structures of two gratings
- The resultant dispersion due to the combination of the two like gratings with the line structures thereof rotated before assembly so that the angle between the grating lines is α is given by the mathematical expression,
- $$(1) \quad \delta_o - \delta_p = (\Delta_o - \Delta_p) \sin \alpha$$
- wherein $\delta_o = \Delta_o \sin \alpha$
 $\delta_p = \Delta_p \sin \alpha$
- If $D_c - D_p$ represents the dispersion of the prism to be achromatized, D being the deviation of the prism for wavelength λ , then
- $$D_o - D_p = \delta_o - \delta_p$$
- By substituting values of $D_o - D_p$ and $(\Delta_o - \Delta_p)$ (obtained from formula (A)) in formula (1) and solving for α , the relative inclination of the line structure of the gratings 22F and 22R may be determined.
- In either of the disclosed forms of the invention, the two gratings are permanently assembled together with a small intervening air space therebetween in an individual cell 17 which also holds the associated prism in spaced relation thereto as shown in Fig. 2, thereby providing a completely achromatized prism in a single small unit. Light may be incident on either side of said unit and the gratings may be placed on either side of the prism with equally good effect.
- As shown in Fig. 5, the aforementioned large deviation of each unit which is inherent in the invention is advantageously utilized by rotatably mounting two of the prism units 17 and 17¹ face to face in a Risley type mounting 18 to form a compensator which transmits white light. By means of bevel gears 19 and 20 fixed on the inner ends of the cells 17 and 17¹, these achromatic systems may be simultaneously rotated in opposite directions by a drive gear 21 meshed with the gears 19 and 20. By this means the deviations of the respective prism units 17 and 17¹ may be combined additively or subtractively to produce all intermediate values of deviation between double and zero deviation of the transmitted spectra.
- As heretofore intimated, each unit 17 and 17¹ may be used reversibly since the light may be incident on either side. Various arrangements of the constituent parts may be used such as placing the prism on one side or the other of the two gratings or placing the prism between the two gratings. The intervening space between both gratings and between the associated prism may be large if desired so long as the effective size of the aperture of the optical system in which these parts are used is made large enough to pass the required amount of light. In any operative arrangement, the gratings should preferably face in the same direction and the placement of each grating should preferably be substantially parallel to a single refractive face on the prism to be compensated, although an operative achromatic system may be provided by locating the ruled surfaces of the gratings parallel to the plane lying within the angle "a" of Fig. 1 as mentioned heretofore. Furthermore,

- the angle between the line structure of one grating and the base of the prism or corresponding part should be the same as the angle between the line structure of the other grating and the base of the prism or corresponding part. In the first described form of this invention, said angle is zero degrees for both gratings and in the second described form, the line structures of the two gratings are rotated by the same amount in opposite directions so as to establish the same angle (\rightarrow) between the base of the prism and each of the line structures.
- It will be observed that the present invention provides effective grating means for completely achromatizing the light transmitted by deviation prisms of various kinds and furthermore the gratings may be variously constructed and arranged with respect to the associated prism so as to compensate for extensive ranges of chromatic aberrations by optical prisms.
- WHAT WE CLAIM IS:—**
1. An achromatic system comprising a light dispersing prism, a pair of diffraction gratings spaced from each other and positioned in optical alignment with said prism, the blaze of one grating being deviated in an opposite direction to the blaze of the other grating to produce a residual dispersion which substantially compensates for the dispersion of the prism.
 2. An optical system according to Claim

1 in which the gratings produce maximum energy in the first order spectra and are positioned so that the respective directions of their maximum energies are symmetrical with the direction of the maximum energy emerging from the prism.

35

3. An optical system according to any one of the preceding claims in which the line structure of both gratings lie at the same angle to the base of said prism.

40

4. An optical system according to any one of the preceding claims, in which the plane of each grating is substantially parallel with a single face of the prism, the line structure of at least one grating extending in a direction parallel to the base of said prism.

45

5. An optical system according to any one of the preceding claims, in which the gratings are arranged in planes which are parallel with the adjacent face of the prism, one of the gratings being rotatable so that it may be set with its line structure at such a predetermined angle to the line structure of the other grating that the vector sum of the opposite deviations of the two gratings is made equal to the dispersion of said prism.

50

6. An optical system substantially as hereinbefore described and as illustrated in the accompanying drawings.

55

STEVENS, LANGNER, PARRY &
ROLLINSON,
Chartered Patent Agents,
Agents for the Applicants.

833,382 COMPLETE SPECIFICATION

1 SHEET

This drawing is a reproduction of
the Original on a reduced scale.

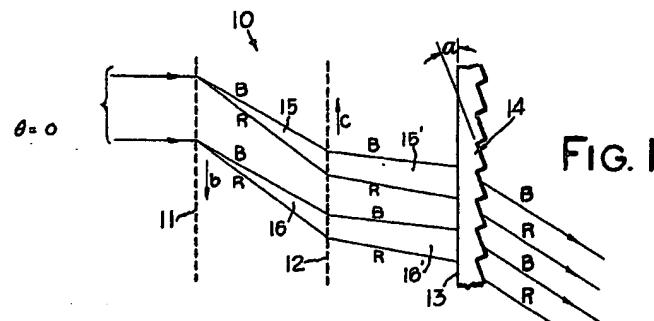


FIG. 1

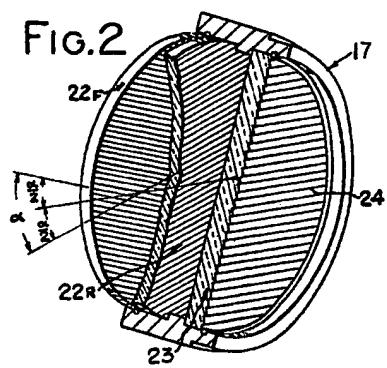


FIG. 2

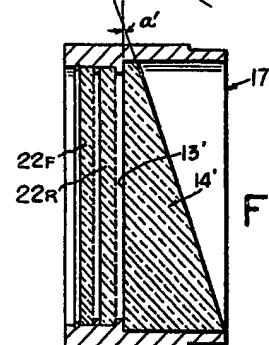


FIG. 3

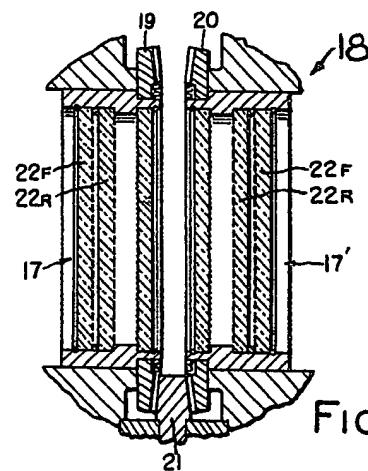


FIG. 5

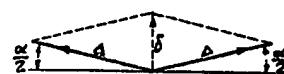


FIG. 4